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Near-field laser parallel nanofabrication of arbitrary-shaped patterns

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The authors present a simple and efficient technique for laser writing of arbitrary nanopatterns across a large surface area without using projection masks. It is based on the unique near-field focusing effect of a self-assembled particle array on the surface interacting with an angular incident laser beam. The spot resolution can be down to 80 nm. More than 6×10^6 nanolines and c-shaped uniform patterns were fabricated simultaneously over an area of 5×5 mm² by a few laser shots. © 2007 American Institute of Physics. [DOI: 10.1063/1.2748035]

Laser-induced surface nanopatterning has become increasingly important due to the rapid development of nanoelectronics, nanophotonic, and biomedical devices.¹ Due to the optical diffraction limit, light cannot be confined to a lateral dimension smaller than roughly one-half of wavelength.² In order to overcome this barrier, near-field optics has attracted much attention in recent years, where evanescence wave becomes significant. So far, several near-field patterning techniques exist: near-field scanning optical microscope (NSOM) patterning,³⁻⁵ laser-assisted atomic force microscopy/scanning tunneling microscopy (AFM/STM)-tip patterning,^{6–8} contacting particle-lens array (CPLA) patterning,^{9–13} and plasmonic lithography (PL).^{14,15} As nearfield techniques, their working distances are in the submicron scale, typically from zero (contacting mode) to several hundreds of nanometers. In NSOM and AFM/STM systems, sophisticated hardware systems were used to control the nearfield distance. In addition the throughput is too low to be used in an industrial environment, as they are serial writing techniques. In CPLA systems, the particle lens is in contact with the surface while in PL system the near-field distance is controlled by spin coating of a transparent spacer layer.¹⁵ The CPLA technique employs a regular two-dimensional array of small particles as lens array, which converts a laser beam into a multiplicity of enhanced optical spots in parallel at focus. Unlike fabrication of conventional microlens arrays by complicated processes such as photolithography and resist reflow, the particle-lens array can be easily prepared by a self-assembly process.^{9,16} The existing CPLA technique is, however, a single-angle processing technique, in which the laser beam is incident perpendicularly to the surface and most of the particles are removed after a single shot.¹⁷ The disappearance of the particles makes it impossible to fabricate complex array patterns other than a hole/cone array. To enable the fabrication of different user-defined nanostructures such as nanolines, we report in this letter a step change of the existing CPLA technique by using an angular scanning laser beam scanning through the particle-lens array on the surface, and demonstrated laser parallel writing of different profiled nanofeatures simultaneously in a large surface area.

In the experiments reported here, a KrF excimer laser (GSI-Lumonic IPEX848) was used as the light source (λ = 248 nm, τ =15 ns, and repetition rate of 1 Hz; nonpolarized). The sample was a 20-nm-thick eutectic Sb₇₀Te₃₀ film coated on a polycarbonate substrate. Monodispersed 1.0 μ m spherical silica (SiO₂, Duke Scientific) particles were diluted with de-ionized water and applied to the film surface. After the water evaporates, a hexagonally closed-packed monolayer was formed on the surface due to the self-assembly process. The sample was then processed and characterized by field-emission environmental scanning electron microscopy (SEM; Philips XL32) and AFM (Vecco CP2).

Figure 1(a) shows a schematic diagram of the basic con-



FIG. 1. (Color online) Schematic diagram of (a) the experimental configuration for direct laser writing of nanoline array on substrate surface, and (b) SEM image of two hexagonal nanodent arrays ablated by a single KrF laser pulse at an incident angles of 0° , with fluence of 6.5 mJ/cm², and 30°, with fluence of 1.0 mJ/cm², respectively.

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cept for laser writing of an array of nanolines on a surface. The laser beam was scanned in the *xz* plane about the *y* axis from a large angle α_1 to a smaller angle α_2 ($\alpha_1 > \alpha_2 > 0^\circ$). It was found that at low-to-medium laser fluences (typically $<10.0 \text{ mJ/cm}^2$) and at angles $\alpha \ge 5^\circ$, most of the particles remain on the surface after processing. The phenomena can be attributed to the fast decay of the intensity peaks on substrate (points P_n in Fig. 1).¹⁷ The shift of these peak positions away from the contact point C with a distance close to that given by the geometrical optics $d \cong r \tan(\alpha)$, where r is the radius of the particle, was experimentally demonstrated in a previous paper.¹⁰ As particles remain on the surface, multiangle processing is possible. To prove this, two-angle processing was demonstrated. The first laser pulse was incident on the sample surface at $\alpha = 30^{\circ}$ (1.0 mJ/cm²) while the second laser pulse at $\alpha = 0^{\circ}$ (6.5 mJ/cm²). Figure 1(b) shows the SEM image of the nanodent arrays ablated by the two-angle processing. As can be seen, the diameter of the nanodents obtained at $\alpha = 30^{\circ}$ (~80 nm) is much smaller than those obtained at $\alpha = 0^{\circ}$ (~300 nm) and is beyond the diffracted resolution of $\sim \lambda/2 = 124$ nm. Such resolution was attained because of the dominance of the evanescent wave modes over free wave modes in the vicinity of the particle, revealing the near-field nature of the technique.¹ To understand the underlying physics of the multiangle processing, the optical near fields around the particle were simulated by a rigorous particle on surface model. The details of the theoretical formulation of the problem can be found in a previous publication.¹⁰ Figure 2 shows the calculated optical near fields in (a) the xz plane for $\alpha = 30^{\circ}$ and (b) along the x direction on film surface for $\alpha = 0^{\circ}, 30^{\circ}, 45^{\circ}$, and 60° . It can be seen from Fig. 2(a) that the Poynting field was not confined to the contact region, but in some region between the particle and the substrate along the incident path. The field maxima were located on the particle surface (point F) and the intensity drops quickly from it. The decay length along the incident path can be written as

$$l_{\text{decay}} \approx r \left(\frac{1}{\cos \alpha} - 1 \right).$$
 (1)

For $\alpha \leq 75^\circ$, l_{decay} is within submicron scale and at $\alpha = 60^\circ$, the $l_{decay} \approx r = 500$ nm. At these distances, the evanescent wave modes play the dominating role and the total fields are enhanced. As can be seen in Fig. 2(b), the peaks of the enhancement factor for the z component of the Poynting field on the sample surface decay quickly with angle. The tendency can be thought as the result of the increasing decay length [as in Eq. (1)] for large angles. Comparing with an exponential decay rate along the incident path in Mie theory, we observed a slower decay rate in Fig. 2(b) because of the multiple scattering and reflection processes between particle and substrate.^{17–19} On the other hand, the peak width in Fig. 2(b) increases with incident angles. At $\alpha > 45^{\circ}$, the full width at half maximum of the peaks is almost two times of those at $\alpha < 45^{\circ}$, indicating a worse pattern resolution at large angles $\alpha > 45^{\circ}$. Due to the symmetric nature of a sphere, point P_3 [as in Fig. 1(a)] can be reached either by a beam incident at an angle of $\alpha_3 > 45^\circ$ with respect to the origin O or by a beam at the angle of $\beta = (90^{\circ} - \alpha_3) < 45^{\circ}$ with respect to the origin O_1 . The worsening resolution problem at large angles can, thus, easily be avoided by changing the incident direction.



FIG. 2. (Color online) Optical near fields in (a) the *xz* plane around a 1.0 μ m SiO₂ sphere situated on the sample surface, illuminated by a 248 nm laser at 30°. The white color in (a) represents the field enhancement value greater than 40. Only the field out of sphere was modeled. The *z* component of the Poynting field on film surface for different incident angles was illuminated in (b).

To form a continuous line, multiangle processing is necessary. The angle scanning resolution was set at 5° , and a single laser pulse was used for each angle. It produced an array of nanolines with characteristic lengths given by:

$$L \cong r |\tan(\alpha_1) - \tan(\alpha_2)|. \tag{2}$$

The normal incident beam ($\alpha = 0^{\circ}$) was intentionally avoided to prevent particle removal during scanning. It was suggested to be only used at the final stage of the processing to produce ablation at the contact point as well as to remove the particles. Figure 3 shows the (a) SEM image and (b) corresponding two-dimensional AFM profile of an array of lineshaped nanostructures, fabricated by the proposed technique. The angles were controlled at $\alpha \leq 45^{\circ}$ and $\beta \leq 45^{\circ}$. The film was ablated locally when the fluence exceeds the threshold of $F_{\rm th} \approx 23 \text{ mJ/cm}^2$. Due to the optical enhancement effect, the threshold fluence can be reduced to $F_{\rm th}/I_{\rm NEF}$, where $I_{\rm NEF}$ represents the normalized enhancement factor, as shown in Fig. 2(b). To obtain minimized spot size on the surface, one has to work at a low laser fluence regime where a higher enhancement factor ($I_{\text{NEF}} \approx 25$ at 30°) is needed to reach the material ablation threshold. In order to produce lines with uniform lateral dimension $(\delta_1 \approx \delta_2 \approx \delta_3)$ by the angular scanning beam, we found that the laser fluences should be controlled within the regions $3 \le I_{\text{NEF}} \le 20$, as marked in Fig.



FIG. 3. (Color online) SEM image (a) and AFM profile (b) of an ordered array of line structures fabricated by the angular scanning technique. The average line length and width are 1400 and 360 nm, respectively. Relative particle positions were marked by dashed circles. In (c) the scanning path is along the angle φ , as in Fig. 1, and it produces an array of c-shaped nanostructures.

2(b). The line array in Fig. 3(a) was fabricated with a laser fluence of $F \approx F_0/\cos(\alpha)$, where $F_0=7.0 \text{ mJ/cm}^2$. It corresponds to an enhancement factor of $I_{\text{NEF}} \approx 3.3$ in Fig. 2(b). The produced line array has a width of around 360 nm. Due to the thermal effect of nanosecond laser pulse ablation, some neighboring nanolines are linked together. The maximum ablation depth is 20 nm and the depth profile in Fig. 3(b) reveals a smaller depth for a larger angle, which can be explained by a lower enhancement peak at a larger angle $[h_1 > h_2 > h_3$ in Fig. 2(b)]. To obtain lines with uniform depth, one can either vary the laser fluence or use multiple laser pulses at each angle. As the particle diameter is $1.0 \ \mu\text{m}$, the number of nanolines over an area of $5 \times 5 \ \text{mm}^2$ exceeds 6×10^6 in our experiments.

It is important to note that the proposed technique is not limited to producing nanoline arrays. It is flexible enough to design the laser scanning path in different planes. For example, one can scan the beam with a fixed angle $\alpha = 45^{\circ}$ but rotate it along the φ angle path [see Fig. 1(a)]. As a result, it produces an array of c-shaped nanostructures, as shown in Fig. 3(c). User-defined complex shape nanopatterns can be easily fabricated (within regions $d \le a$) by designing the laser scanning path, which would be far easier to realize than direct writing by controlling the perpendicularity between lens arrays and substrate in nanoscale.²⁰ Since particles can be deposited on a nonflat surface, the technique can be extended to generate patterns on a rough or even curved surface. As a final note, the technique can be further developed by using femtosecond lasers as the light source to improve the patterning resolution down to sub-50-nm scale and to pattern samples with higher ablation threshold, due to its unique properties in laser ablation.^{21,22} The developed technique is simple, low cost, and efficient which offers great potential for large scale industrial applications.

In summary, we have demonstrated an efficient laser nanoprocessing technique to produce multiple complex nanofeatures simultaneously on solid surfaces. Each particle in the array works as a near-field focusing lens and the focusing position can be precisely tuned by the incident angle, making it possible to fabricate any user-defined nanostructure. Uniform lateral dimension can be achieved by choosing an appropriate laser fluence.

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